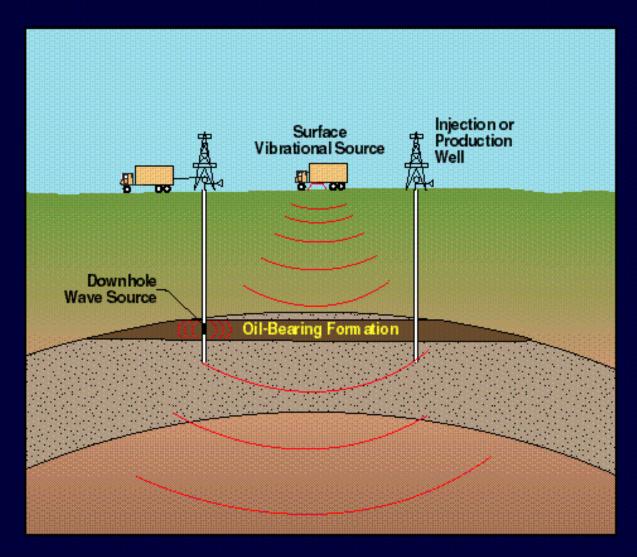
SEISMIC STIMULATION FOR ENHANCED PRODUCTION OF OIL RESERVOIRS



Downhole or surface seismic sources generate low-frequency (1 - 500 Hz) waves that interact with the reservoir formation and fluids to increase the oil production rate and/or total oil recovered.

MEETING OBJECTIVES

- Review status and plans for DOE research
- Update (voluntary) on industry activities
- Define major problems and unknowns
- Identify short and long term project goals
- Define roles of LANL, LBNL and industry
- Project administrative issues
 -procedure for new companies joining
 -propose industry representative(s)

SEISMIC STIMULATION FOR ENHANCED PRODUCTION OF OIL RESERVOIRS

Current Industry Participants:

Chevron, Conoco, Fluidic Technologies, Halliburton, Marathon Oil, Oil and Gas Consultants Intl. PerfClean Intl., Phillips Petroleum, Piezo Sona-Tool, Reservoir Stimulation Technology, Texaco, Wave Energy Resources

DOE Participants:

Los Alamos National Laboratory
Lawrence Berkeley National Laboratory

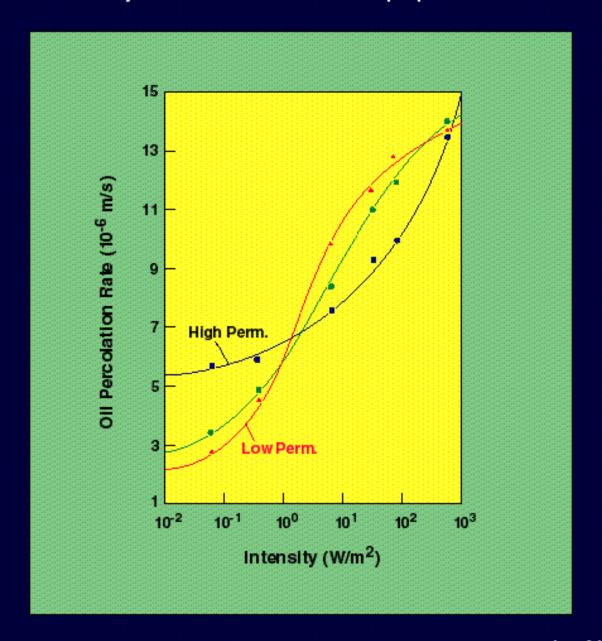
SEISMIC STIMULATION FOR ENHANCED PRODUCTION OF OIL RESERVOIRS

Background:

- Roughly 60% of domestic oil remains unproduced.
- Seismic waves can increase oil production.
- 50% or more increase in recovery is possible.
- Field tests give widely varying results.
- Laboratory data are inconclusive.
- Stimulation mechanisms are poorly understood.
- More basic R&D needed to increase field success.

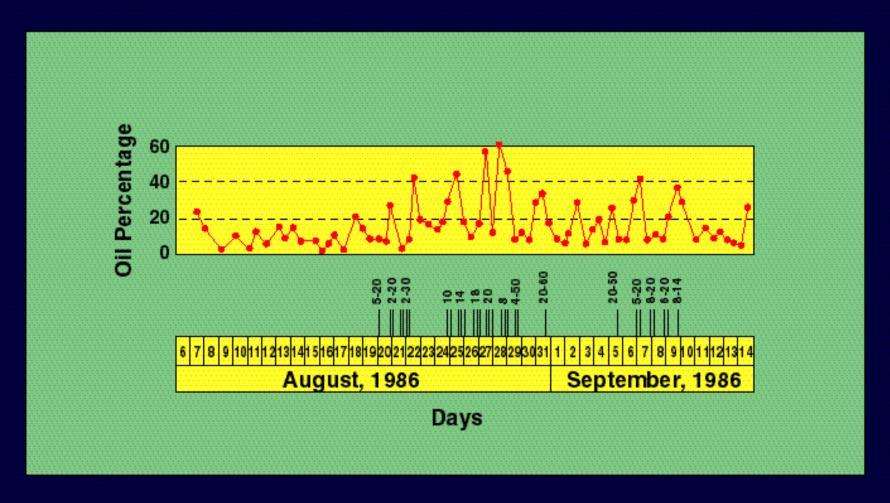
Ashiepkov (1989)

Oil percolation rates through sandstone versus applied acoustic intensity at 30 - 400 Hz for 3 initial sample permeabilities.



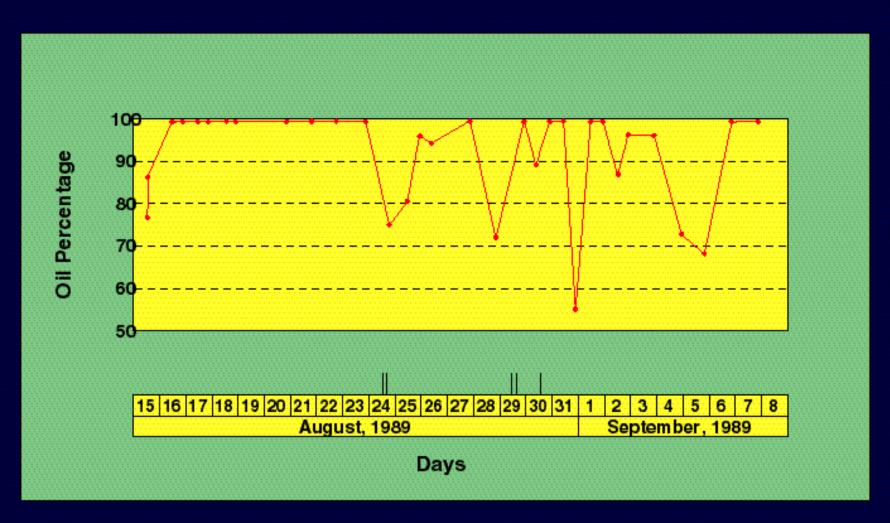
Kissin (1991)

Effects of 20-ton Vibroseis stimulation on the oil percentage of produced fluid from a depleted reservoir in the Northern Caucasus. Reservoir was 1200 m deep and 10 m thick.



Nikolaev & Kuznetsov (1990)

Effects of 20-ton Vibroseis stimulation on the oil percentage of produced fluid from a productive reservoir. Initial oil cut was close to 100%. Stimulation was applied at approximately 20 Hz.



Possible Mechanisms of Enhanced Oil Production

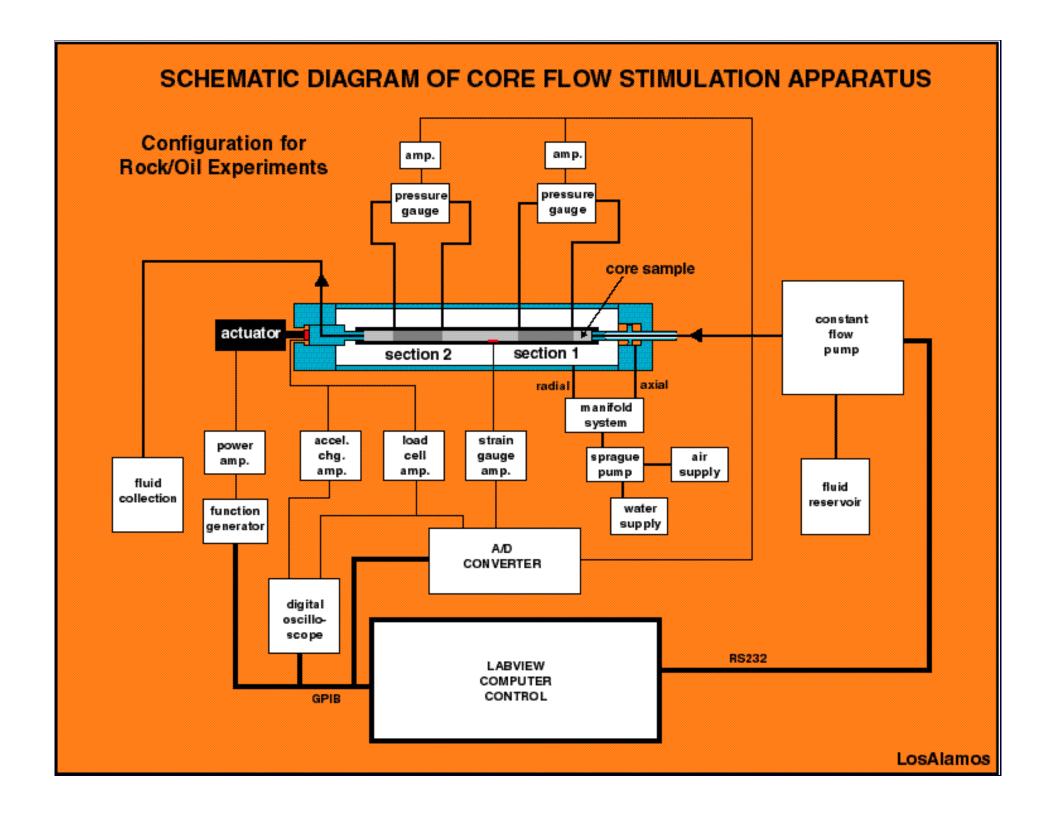
Low-Frequency Stress Waves May:

- increase absolute permeability by destroying pore wall boundary films or liberating in-situ fines
- reduce residual oil saturation by coalescence of dispersed oil droplets
- mobilize oil trapped in low-permeability zones inaccessible to water floods
- increase relative permeability of oil during 2-phase oil/water flow

SEISMIC STIMULATION FOR ENHANCED PRODUCTION OF OIL RESERVOIRS

Research Focus Areas:

- Laboratory core flow experiments.
- Numerical and theoretical modeling.
- Field experimental testing.







CORE STIMULATION LABORATORY CAPABILITIES

PARAMETERS

VALUES

SAMPLE TYPE

uniform permeability non-uniform permeability differing fines content field core samples unconsolidated samples

1-inch diameter up to 24 inches long Young's mod. ≤ 10⁷ psi permeability: 1 - 500 md saturation: 0 - 100%

STATIC LOADS

triaxial confinement Hassler confinement fluid back pressure fixed or free back end

radial stress ≤10,000 psi axial stress ≤10,000 psi fluid press. ≤9,000 psi

FLOW MODES

pulse-free flow rates single phase two phase im bibition drainage

flow: .02 - 800 cc/min pressure ≤ 6,000 psi 2-phase ratio: 0-100% various fluid viscosities various fluid densities

STIMUL. MODES

axial stress cycling axial displacement pore pressure pulsing

frequency: DC - 2 kHz strains up to 10⁻⁴ displacement ± .002 in dynamic force ± 200 lbf fluid pulse to 100 Hz fluid pulse to 1000 psi

EXPERIMENTAL MEASUREMENTS

absolute permeability
relative permeability
production rates
residual saturation
mechanical stress, strain
pore pressure fluctuation

LAB EXPERIMENTS PLANNED FOR FY98

SAMPLES:

- Berea Sandstone
- Fontainbleau Sandstone
- Carbonate Rocks
- Diatomite
- Unconsolidated Sand
- Synthetic Cores

EFFECTS:

- Absolute Perm.
- Relative Perm.
- Production Rate
- Residual Saturation
- Fluid Mobilization
- Wave Parameters

CORE FLOW STIMULATION EXPERIMENTS PERFORMED

- Absolute permeability enhancement (2 Berea and 1 sand sample)
- Reduction of residual decane saturation after drainage and imbibition
- Mobilization of trapped DNAPL in a sand core during water flood
- Reduction of permeability damage caused by fines migration in Berea

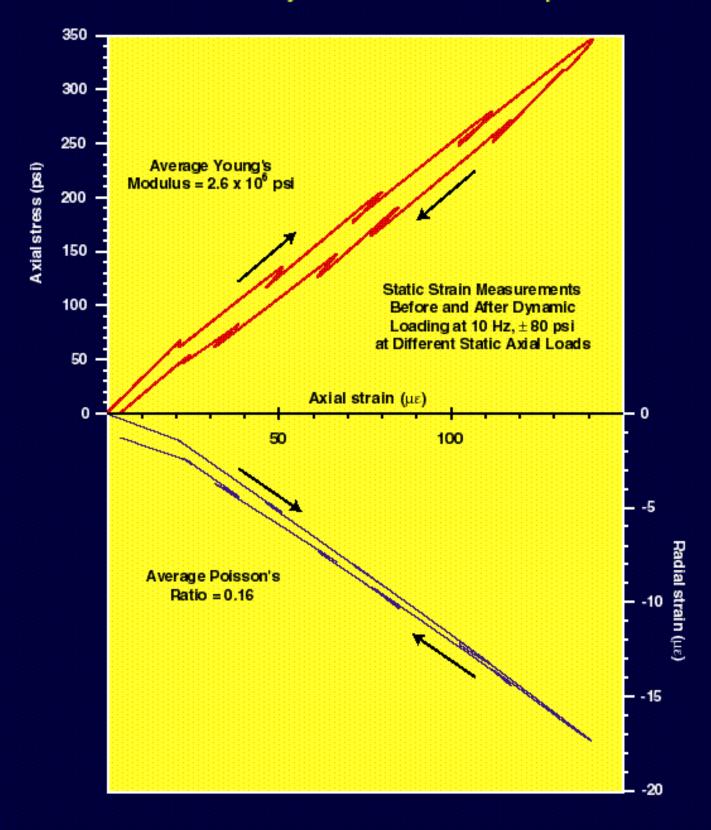
BEREA SANDSTONE SAMPLE PHYSICAL AND ELASTIC PROPERTIES

- Diameter: 0.98 in (2.5 cm)
- Length: 12.56 in (31.9 cm)
- Cross-Section Area: 0.751 in² (4.8 cm²)
- Total Volume: 155 mL
- Connected Pore Volume: 38 mL
- Connected Porosity: 0.24
- Nominal Permeability: 500 md
- Saturated Density: 149 lb/ft³ (2390 kg/m³)
- Acoustic Velocity: 7900 ft/s (2400 m/s)
- Young's Modulus: 2.6 x 10⁶ psi (18 GPa)
- Poisson's Ration: 0.16

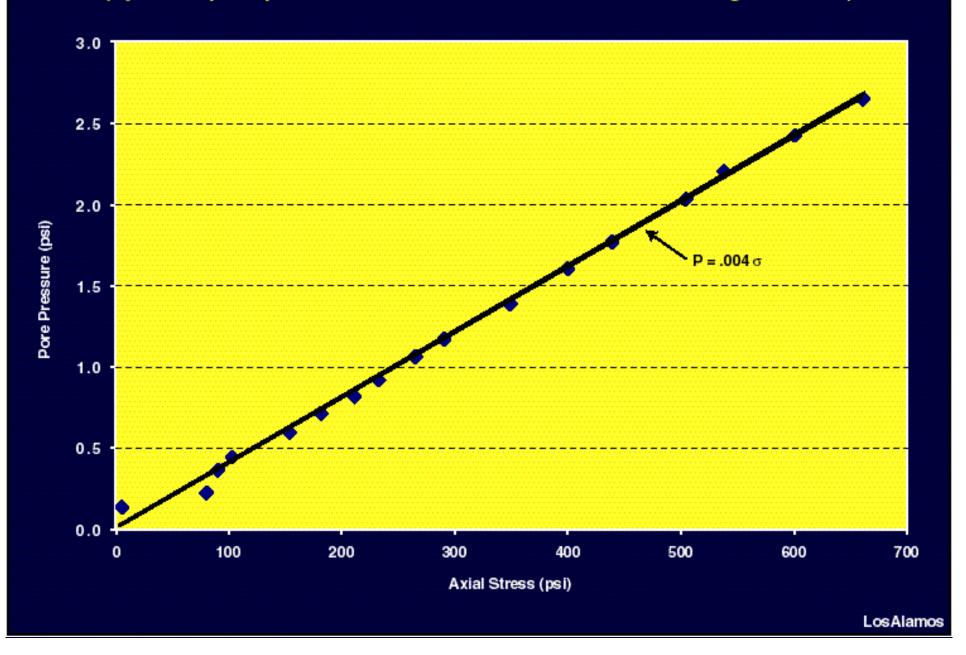
TYPICAL STIMULATION PARAMETERS USED FOR BEREA EXPERIMENTS

- Frequency Range: 50 100 Hz
- Axial Load: ± 60 lbf (267 N)
- Axial Stress: ± 80 psi (0.5 MPa)
- Axial Strain: ± 60 με
- Axial Displacement: ± 0.001" (20 μm)
- Axial Acceleration: ± 0.2 g (2 m/s²)
- Pore Pressure: << 0.3 psi (2 kPa)</p>
- Acoustic Intensity: 0.1 W/m²

Axial Stress and Radial Strain vs. Axial Strain Curves for Dry Berea Sandstone Sample



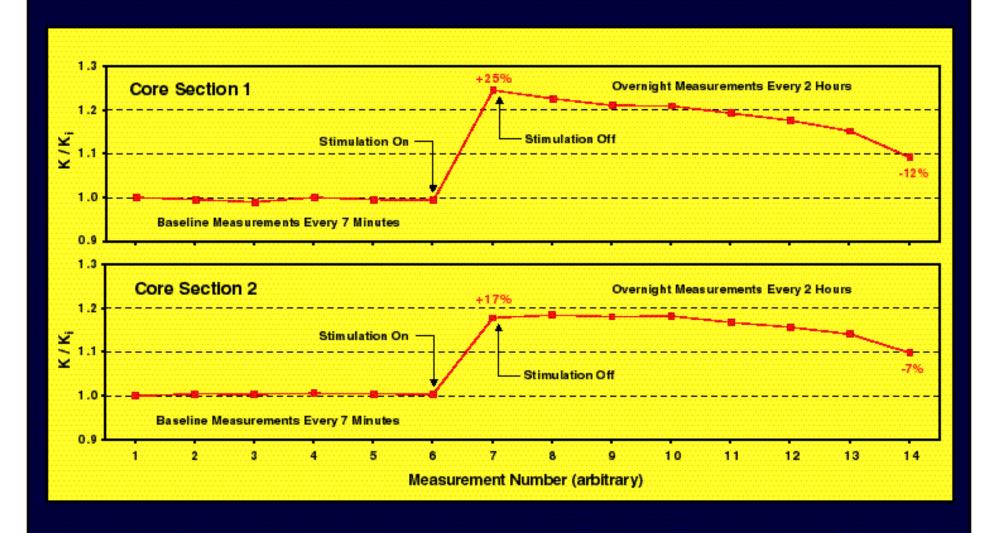
Maximum Static Fluid Pore Pressure vs. Axial Stress for Sealed System (dynamic pore pressure is more than 10 times lower during fluid flow)



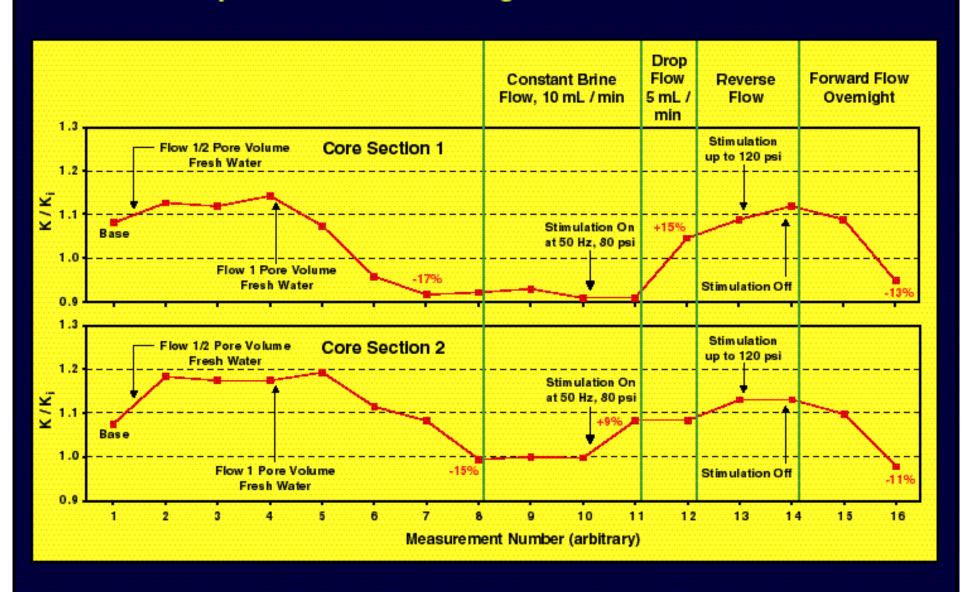
BEREA PERMEABILITY AND FINES EXPERIMENTAL PROCEDURE

- Confine core at 1000 psi radial and 800 psi axial
- Evacuate sample and saturate with brine
- Start brine flow and measure initial permeability
- Stimulate and measure permeability changes
- Liberate clay fines by briefly flowing fresh water
- Resume brine flow and measure permeability drop
- Stimulate to mobilize fines and restore permeability
- Change flow rate and direction during stimulation

Permeability Changes Observed in 2 Core Sections Before, During and After 10 Minutes Continuous Stimulation at 50 Hz Frequency and \pm 80 psi Axial Stress



Permeability Changes Caused by Fresh-Water Fines Mobilization Followed by Stress Stimulation during Forward and Reverse Brine Flow



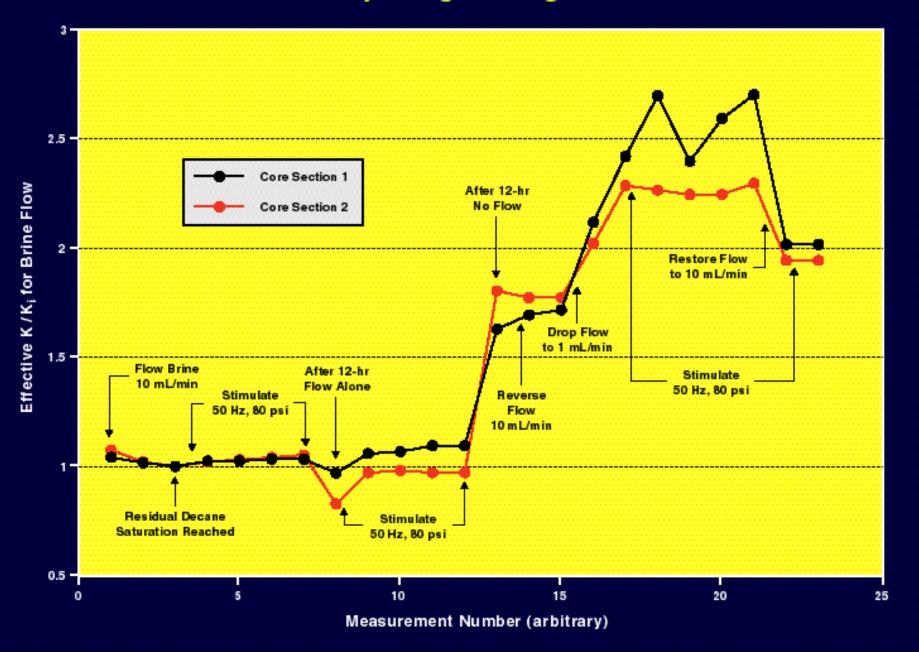
DECANE-BRINE DRAINAGE / IMBIBITION EXPERIMENTAL PROCEDURE

- Start with core initially brine saturated
- Drainage with decane until no more brine produced
- Stimulate to try decreasing S_{RW}
- Imbibition with brine until no more decane produced
- Stimulate to try decreasing S_{RO}
- Repeat drainage / imbibition cycle
- Change flow rate and direction during stimulation
- Measure effective permeability changes

DECANE-BRINE DRAINAGE / IMBIBITION SATURATION AND PERMEABILITY HISTORY

flow operation	core fluid content after each run				effective perm. (md)	
	brine		decane		to flowing phase	
	mL	%P.V.	mL	%P.V.	section 1	section 2
brine sat.	37.8	100	0	0	689	789
drainage	9.5	25	28.3	75	638 - 678	617 - 698
imbibition	27.0	71	10.8	29	104 - 226	126 - 257
drainage	9.8	26	28.0	74	593 - 650	801 - 812
imbibition	26.2	69	11.6	31	90 - 185	99 - 228

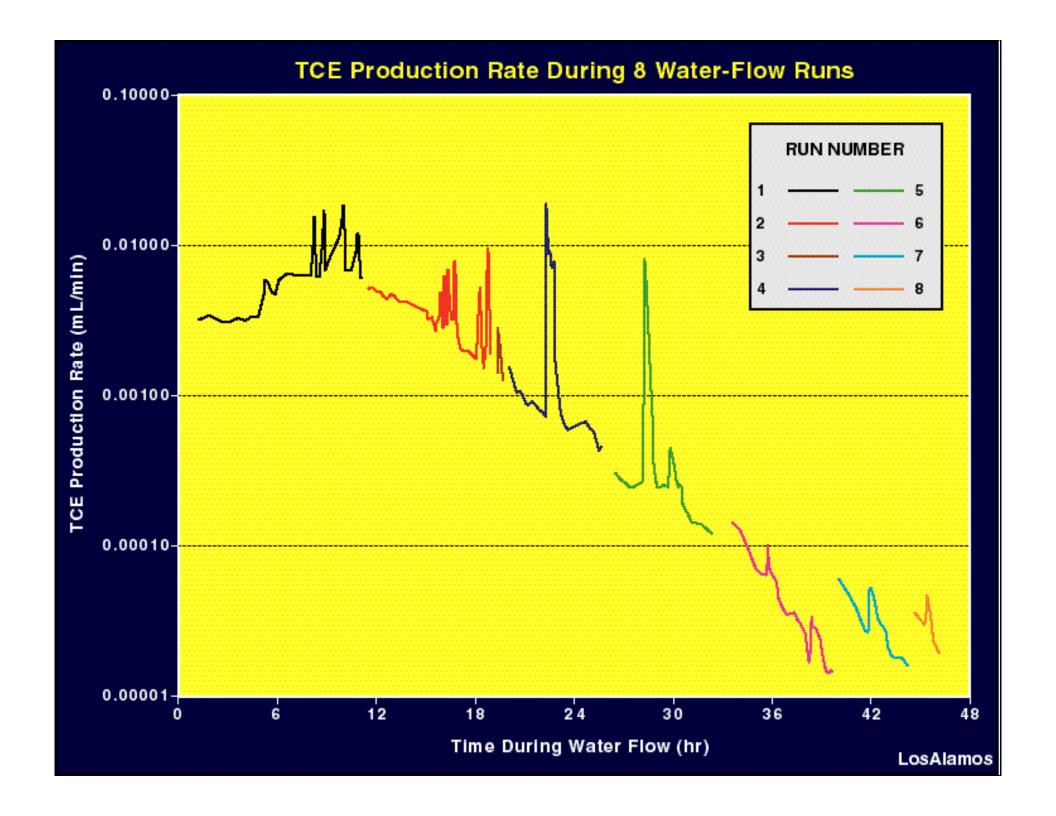
Effective Permeability Changes During 2nd Imbibition Run

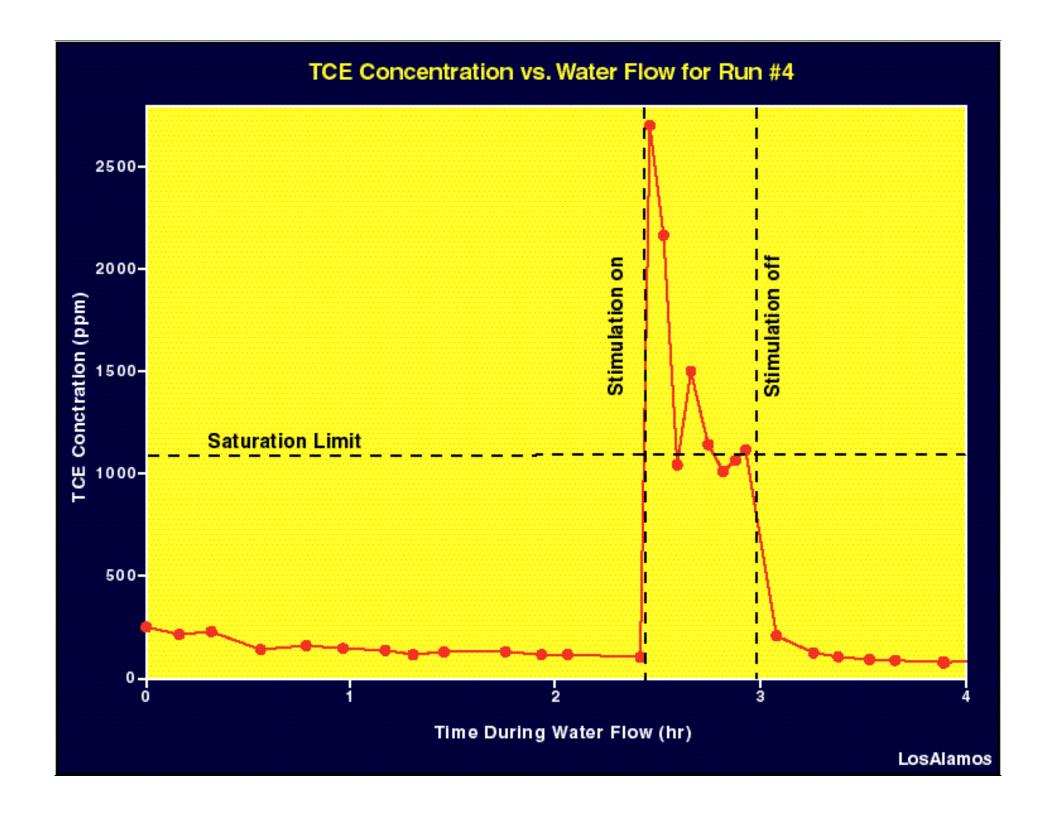


SCHEMATIC DIAGRAM OF CORE FLOW STIMULATION APPARATUS Configuration for amp. am p. Sand/TCE Experiment TCE diff. abs. injection pressure pressure SAND CORE constant actuator flow pump axial radial manifold system actuator accel. power current charge sprague air amp. probe amp. pump supply fluid reser voir function water generator supply digital oscilloscope RS232 fluid GPIB collection ANALOG INPUTS DAQ COMPUTER CONTROL card LosAlamos

TCE PRODUCTION ENHANCEMENT EXPERIMENTAL PROCEDURE

- Pack sand into sleeve and apply confinement
- Evacuate sample and saturate with water
- Inject 10% pore volume of TCE into sand
- Initiate pulse-free flow of water through sand
- Measure effluent TCE concentration with GC
- Stimulate and measure TCE production change
- Measure applied displacement and pressure





TCE Concentration vs. Water Flow for Run #5

